

DRIVER FOR AN ULTRASONIC TRANSDUCER AND AN ULTRASONIC
TRANSDUCER

Background of the Invention

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1. Field of the Invention

The invention relates to drivers for ultrasonic transducers and to ultrasonic transducers. In particular the invention relates to a driver and ultrasonic transducer for use as a bonding apparatus in wire-bonding machines.

2. Description of Prior Art

Ultrasonic transducers on wire-bonding machines are used to apply pressure and ultrasonic energy simultaneously for connecting the lead wires from a semiconductor component to a substrate. The ultrasonic transducer has an ultrasonic driver for converting driving signals from an ultrasonic signal generator into ultrasonic vibrations. A horn amplifies the ultrasonic vibrations from the driver and a bonding tool, which is normally in the form of a wedge or a capillary, located at the smaller end of the horn couples the amplified ultrasonic vibrations while applying a predetermined bond force to the lead wires and components being bonded together. Piezoelectric materials

are used as the active (or driving) materials in the ultrasonic driver. It is difficult to induce electric polarization in thick piezoelectric elements and so a plurality of piezoelectric elements are stacked up to 5 achieve the desired power level.

FIG 1 shows a collapsed view and an exploded view of a prior art ultrasonic driver. The driver comprises a plurality of ring-shaped piezoelectric elements 1, 1', 10 1'', 1''' connected electrically in parallel and mechanically in series under a mechanical pressure exerted by a pre-stress mechanism formed by a metallic threaded shaft 2 and a metallic nut 3. Thin ring-shaped electrodes 4, 4', 4'', 4''', 4'''' are interposed between the 15 piezoelectric elements 1, 1', 1'', 1''', shaft 2 and nut 3 to provide electrical interconnection and external-connection with an ultrasonic signal generator (not shown).

20 A problem with piezoelectric ultrasonic transducers is that they are subject to accelerated aging and fail when operating at elevated electrical, mechanical and/or temperature stress to increase mechanical power output. These transducers are not considered inherently reliable 25 in high-power applications. Although multiple

piezoelectric elements could be combined or grouped to produce transducers with increased power-handling capability. This would result in inefficient transducers that are not only larger and heavier but also difficult to assemble and costly to operate.

Prior to the use of piezoelectric materials, magnetostrictive transition metals, such as iron (Fe), cobalt (Co) and nickel (Ni) were sometimes used. Although these early transition metals are less susceptible to deterioration under use, they are heavy and bulky. More importantly, their low transduction capability and low energy density significantly limit the mechanical power output from a given electromagnetic power input and volume of the material and so increase the size and weight of the resulting transducer.

Summary of the Invention

It is an object of the present invention to provide a driver for an ultrasonic transducer, and an ultrasonic transducer, for wire bonding applications that has improved power-handling capability, higher efficiency and better reliability, or which at least overcomes or

ameliorates some of the disadvantages of prior art devices.

According to a first aspect of the invention there is
5 provided an ultrasonic transducer driver comprising:

a giant magnetostriictive element,
a fastener for holding the giant magnetostriictive element under mechanical pressure,
a first field generator for providing a magnetic bias
10 field,
a second field generator for providing a magnetic drive field, and
a magnetic circuit for channelling the magnetic fields in the magnetostriictive element.

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According to a second aspect of the invention there is provided an ultrasonic transducer for a bonding apparatus, said transducer comprising:

a horn having a bonding tool at a smaller end and a
20 mounting collar at an opposite end, and
a driver coupled to the horn, the driver comprising a giant magnetostriictive element, a fastener for holding the giant magnetostriictive element under mechanical pressure, a first field generator for providing a magnetic bias field, a second field generator for providing a magnetic
25 field,

drive field, and a magnetic circuit for channelling the magnetic fields in the magnetostriuctive element.

Preferably, the giant magnetostriuctive element is a rare-
5 earth-alloy-based material.

Preferably, the giant magnetostriuctive element is Terfenol-D and its composites.

10 Preferably, the giant magnetostriuctive element is cylindrical with a central hole.

Preferably, the giant magnetostriuctive element is a composite comprising two or more rare-earth-based alloy
15 parts separated from one another by a layer of passive polymeric material.

Preferably, the fastener is a threaded shaft and a nut made of nonmagnetic metallic material.

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Preferably, the first field generator is a permanent magnet.

25 Preferably, the second field generator is an electric coil.

Preferably, the magnetic circuit is a magnetic enclosing circuit having a pair of magnetic return-path rings and a magnetic return-path cylinder made of high-permeability, 5 high-resistivity and high-saturation material.

Further aspects of invention will become apparent from the following description which is given by way of example only.

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Brief Description of the Drawings

Embodiments of the invention will now be described by way of example only and with reference to the accompanying 15 drawings in which:

FIG. 1 shows a collapsed view and an exploded view of a prior art ultrasonic driver,

20 FIG. 2 illustrates an example ultrasonic transducer,

FIG. 3 shows a collapsed view and an exploded view of an ultrasonic transducer driver according to the invention,

25 FIG. 4 is a cross-sectional view of the driver of FIG 3,

FIG 5 is an exploded view of a second embodiment of an ultrasonic transducer driver according to the invention,

5 FIG 6 is an exploded view of a third embodiment of an ultrasonic transducer driver according to the invention,

FIGS 7a to 7f show different configurations of a giant magnetostrictive element for the driver,

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FIG 8 is a plot of electrical impedance against frequency for an embodiment of the present invention made using Terfenol-D/epoxy pseudo 1-3 composite as shown in FIG 7b, and

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FIG 9 is a plot of displacement amplitude against frequency for the transducer of FIG 8.

Description of the Preferred Embodiments

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In the following description the term "giant magnetostrictive material/element" refers to those ferromagnetic materials possessing unusually large magnetostrictive effect as compared with early transition metals, such as iron (Fe), cobalt (Co) and nickel (Ni).

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These giant magnetostriuctive materials are preferably but not exclusively rare-earth-alloy-based materials such as Terfenol-D and its composites.

5 Referring to FIG 2, an ultrasonic transducer consists of an ultrasonic driver 5, an ultrasonic horn 6, a bonding tool 7 and a barrel 8. The ultrasonic driver 5 is a pre-stressed sandwich transducer functioning as a half-wave, longitudinal, mass-spring-mass, linear vibrator to convert
10 the electromagnetic energy generated by an ultrasonic signal generator (not shown) into longitudinal vibrations at ultrasonic frequencies. The ultrasonic horn 6 is used to couple and amplify the ultrasonic vibrations from the driver 5. The bonding tool 7, which is normally in the
15 form of a wedge or a capillary, is clamped into the hole 9 drilled at the smaller end 10 of the horn 6 for coupling and further amplifying the ultrasonic vibrations with the maximum amplitude being located at its tip 11. The barrel
20 8, which is composed of a flange 12 and a collar 13, is for mounting the whole transducer onto a wire-bonding machine so that the predetermined bond force can be applied, together with the ultrasonic vibrations, to the lead wires and components being bonded together via the tip of the bonding tool. The flange part 12 of the barrel
25 8 is mechanically adjoined onto the horn 6 at a specific

location corresponding to a nodal point of the longitudinal vibration (i.e., zero vibration amplitude) in order to avoid loss of energy and hence degradation of bonding performance. The collar part 13 is mechanically 5 extended from the flange part 12 for further decoupling of the horn 6 from the wire-bonding machine. The transducer is mounted to the wire-bonding machine via the collar 13.

Referring to FIG 3 and 4, the driver 5 functions as a 10 half-wave, longitudinal, mass-spring-mass, linear vibrator to deliver ultrasonic vibrations to the adjoined horn 6. It has a giant magnetostrictive element 14 clamped mechanically under pressure by a pre-stress mechanism formed by a threaded shaft 15 and a nut 16 made of a high- 15 strength, nonmagnetic metallic material, such as stainless steel 304, titanium alloys, aluminium alloys, or the like. A pair of ring-shaped permanent magnets 17, 17', which situate at both ends of the magnetostrictive element 14, provide a magnetic bias (or dc) field to the element 14 to 20 produce an initial static mechanical strain. To ensure a uniform distribution of magnetic flux lines, the outer diameter of these magnets is slightly larger than that of the element (i.e., 1.2 times larger) and the diameter to thickness ratio of the magnets is about 12:1.

The magnets 17, 17' are preferably but not exclusively monolithic sintered or polymer-bonded neodymium iron boron (NdFeB) and samarium cobalt (SmCo) magnets. Sintered magnets have higher magnetic properties and better thermal stability, while polymer-bonded magnets provide higher electrical resistivity (i.e., they are less susceptible to eddy-current losses) and lower density. If sintered magnets are employed, it is preferably to provide a slit for the magnets so as to minimize the eddy-currents accumulating on their major surfaces.

A magnetic drive (or ac) field, is supplied by the drive solenoid 18 having any dimensions and any number of turns of enamelled metallic wire (i.e., enamelled copper wire) in one or more layers and surrounding the magnetostrictive element 14 with a finite air gap 19 in between. A magnetic drive (or ac) field provides an oscillating strain centered on the initial static strain. A magnetic circuit, which helps to channel magnetic fluxes into the element, is created with a pair of magnetic return-path rings 20, 20' on each end of the magnetostrictive element-permanent magnet assembly and an external magnetic return-path cylinder 21. The whole circuit is made of a high-permeability, high-resistivity and high-saturation

material, such as powdered metal "T2", mu-metal, iron, nickel, cobalt, or the like.

The giant magnetostriuctive element can be made from a material such as Terfenol-D. Terfenol-D is an alloy of rare-earth elements terbium (Tb) and dysprosium (Dy) and the transition metal iron (Fe). It exhibits giant linear strain (approx. 1200 ppm) and strain energy density (approx. 20 kJ/m³) with an expeditious response (approx. 1 μ s) at both room temperature and low fields (<150 kA/m). These values are about ten times better than piezoelectric materials and about one hundred times better than early transition metals. Furthermore, it is known that piezoelectric materials require an external, high electric "poling" field to induce an electric polarization. This results in a great difficulty in producing thick piezoelectric elements and, thus, stacking up multiple piezoelectric elements to achieve the desired power level is usually adopted in practice. By contrast, there is no need to "pole" these giant magnetostriuctive materials so that a single element with variable dimensions, a more constant performance over time and a simpler fabrication process in device applications can be obtained.

Referring to FIG 5, in second embodiment of the driver the threaded shaft 15 and a monolithic magnetic return-path ring 20 are manufactured into a single component, while the nut 16 is combined with another monolithic magnetic 5 return-path ring 20' to form another single component.

Referring to FIG 6, in a third embodiment of the driver the threaded shaft 15, a monolithic magnetic return-path ring 20 and a monolithic permanent magnet ring 17 are 10 manufactured into a single component, while the nut 16 is combined with another monolithic magnetic return-path ring 20' and another monolithic permanent magnet ring 17' to form another single component.

15 A layer of thick-film or thin-film magnetic return-path and/or a layer of thick-film or thin-film permanent magnet can be coated on the contacting surface of both the threaded shaft 15 and nut 16 by using thick-film technology and thin-film techniques (i.e., sputtering, 20 pulsed laser deposition (PLD), etc.), respectively. This design is advantageous in minimizing the number of components and hence the number of component interfaces appeared in the driver 5, thereby increasing the flexibility of assembly as well as the quality and 25 reliability of the resulting driver 5. In general, giant

magnetostriuctive ultrasonic drivers/transducers require fewer components as compared with piezoelectric ultrasonic drivers/transducers counterparts. This suggests that a driver/transducer according to the invention not only 5 possesses reduced size and weight but is also easier to assemble and cheaper to operate.

FIG 7 shows different configurations of a giant magnetostriuctive element 14 for the ultrasonic driver 5. 10 It is noted that any shape is possible even though a cylindrical shape with a central hole is shown. FIG 7a illustrates a monolithic giant magnetostriuctive element. While usefulness, monolithic materials, being alloys, generally have two disadvantages. The first is the 15 limitation of the operational frequency to a few kilohertz due to the presence of eddy-current losses, while the second is difficulties in machining and fabricating devices owing to the brittleness of the material. By fabricating the monolithic materials into a composite form 20 comprising two or more monolithic parts separated from one another by at least a layer of passive polymeric material (i.e. epoxy), the materials' bandwidths can conveniently be extended into the ultrasonic regime ($>=20$ kHz) and their brittleness can significantly be reduced due to

increased electrical resistivity and mechanical durability, respectively.

FIGS 7b to 7f show a composite giant magnetostriuctive element in different configurations. These composites in turn include, but are not limited to, pseudo 1-3 (i.e., giant magnetostriective particles are aligned longitudinally in the polymer matrix), 0-3 (i.e. giant magnetostriective particles are dispersed randomly in the polymer matrix), 1-3 (i.e., polymeric layers are extended transversely in an orthogonal direction), radial 2-2 (i.e., polymeric layers are extended radially in any direction) and parallel 2-2 (i.e., polymeric layers are extended transversely in a single direction) configurations.

FIG 8 shows a plot of electrical impedance against frequency for an ultrasonic driver using the pseudo 1-3 giant magnetostriective element of FIG 7b made of a Terfenol-D/epoxy composite. The transducer resonates at approx. 64 kHz. Apart from this resonance, the electrical impedance increases essentially linear with increasing frequency, i.e., the transducer behaves like an inductor. This implies that eddy-current losses are insignificant in this transducer for frequencies up to 100 kHz.

FIG 9 is a plot of displacement amplitude against frequency for the transducer of FIG 8. As in FIG 8 the displacement has a flat response up to and beyond the 5 fundamental resonance of the transducer without eddy-current losses. At resonance the displacement amplitude is about 40 times that of the low frequency data, i.e., 1 kHz.

10 By using giant magnetostriuctive materials in the driver, in particular the rare-earth-alloy-based materials such as Terfenol-D and its composites, novel ultrasonic transducers possessing improved power-handling capability with a higher efficiency and a better reliability are 15 obtained for wire bonding applications.